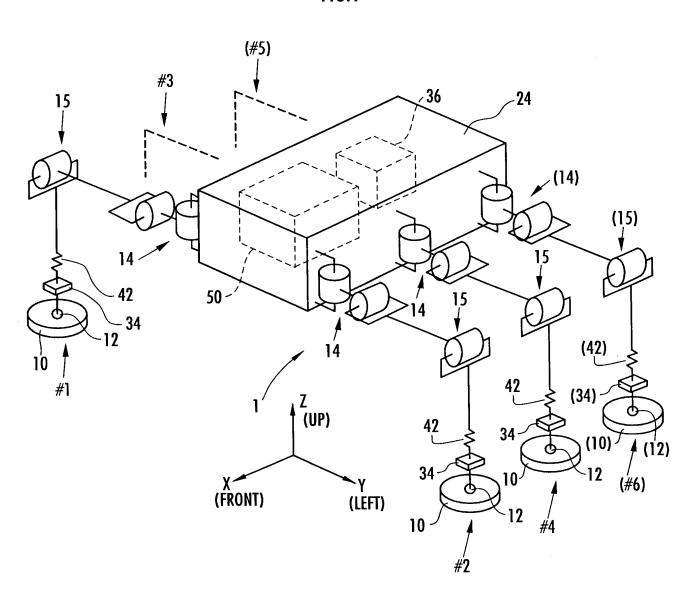
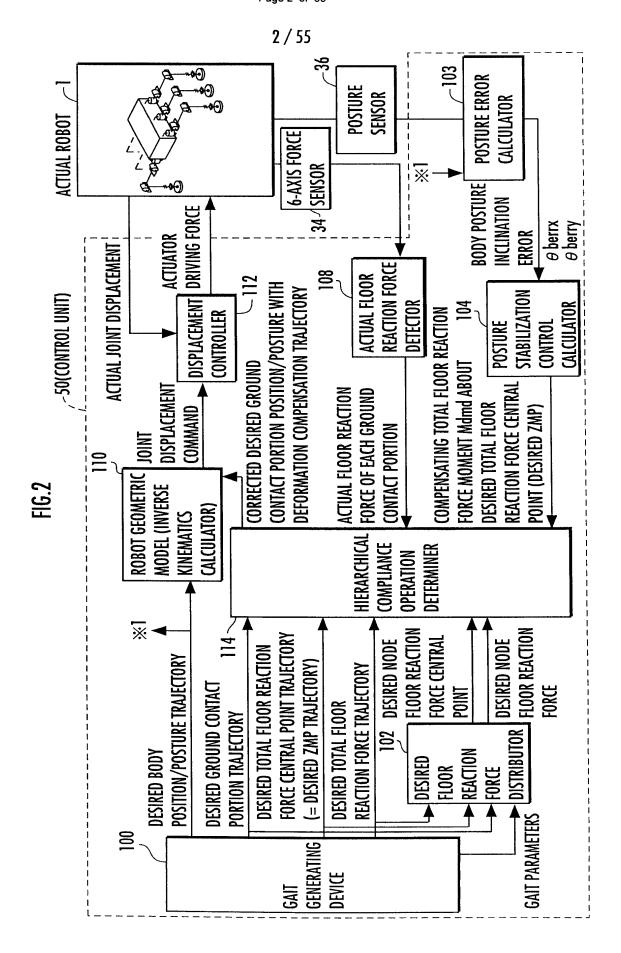
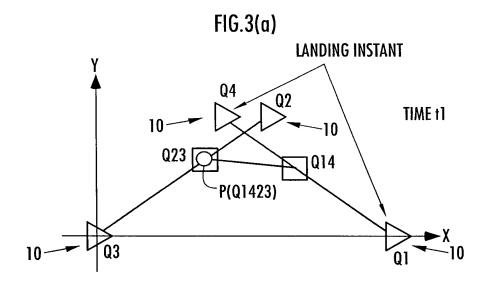
FIG.1

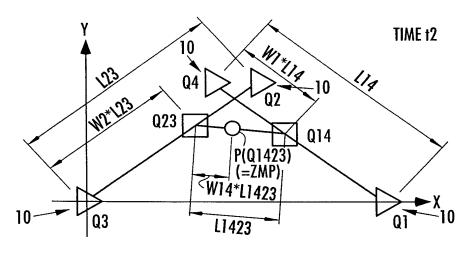


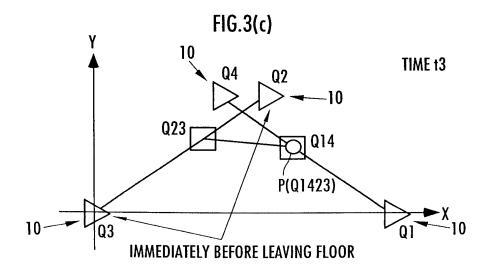


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4 / 55 FIG.4(a)

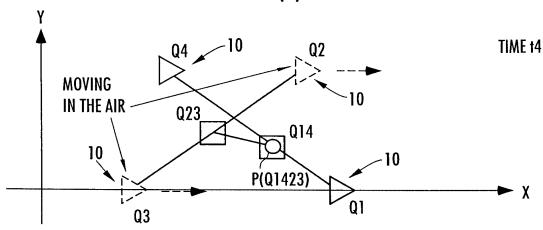


FIG.4(b)

LANDING INSTANT

Q4

10

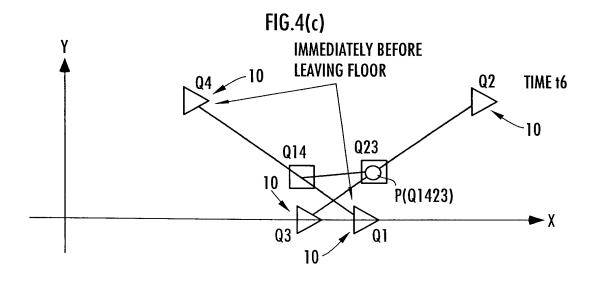
P(Q1423)
Q14

Q23

10

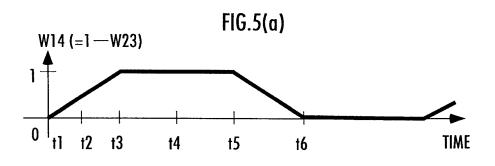
10

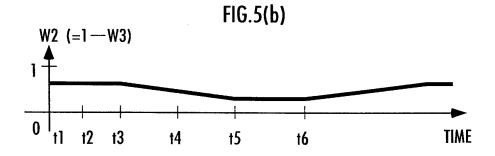
► X

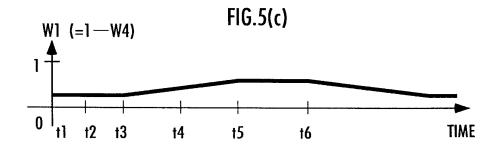


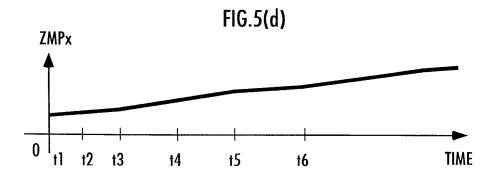
Q3

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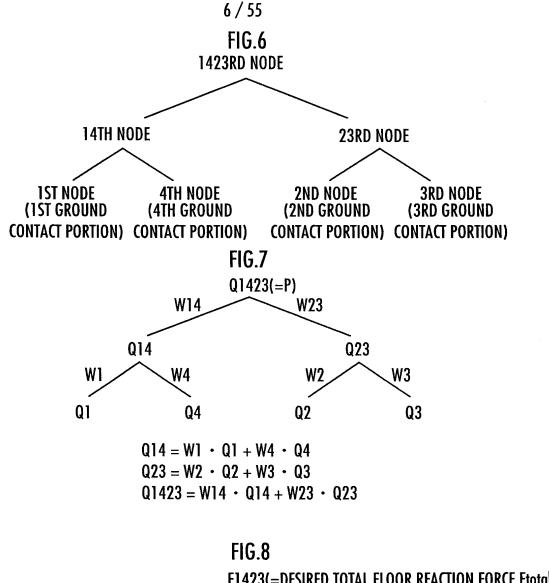






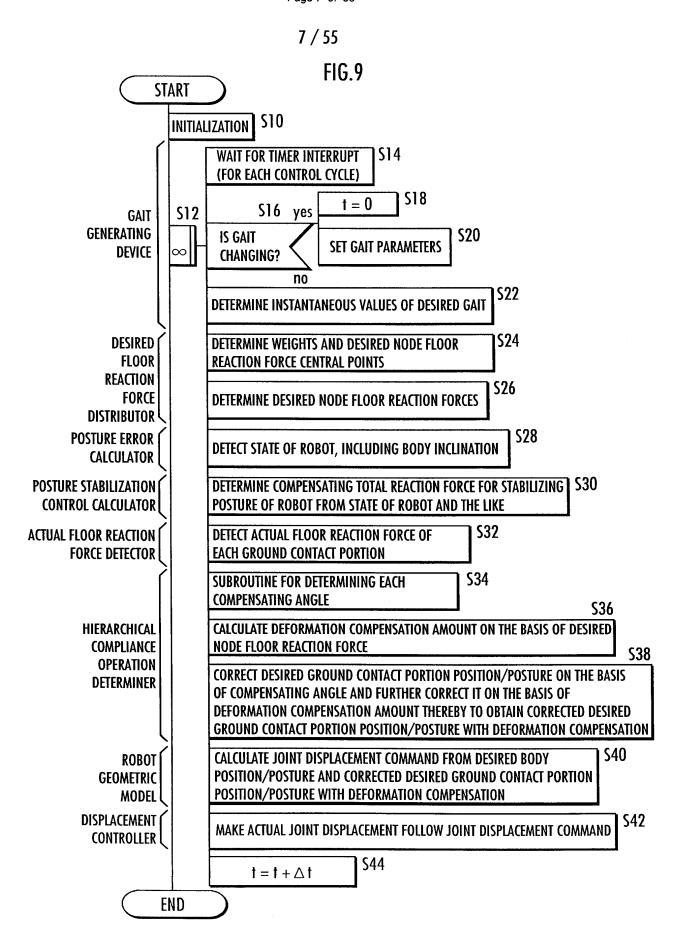


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F1423(=DESIRED TOTAL FLOOR REACTION FORCE Ftotalref) W14 **W23** F14 F23 W1 W4 W2 W3 Fl F4 F2 **F3** F1 = W1 · W14 · Ftotalref F4 = W4 • W14 • Ftotalref F2 = W2 · W23 · Ftotalref F3 = W3 · W23 · Ftotalref F14 = F1 + F4F23 = F2 + F3F1423 = F14 + F23

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8 / 55 FIG.10

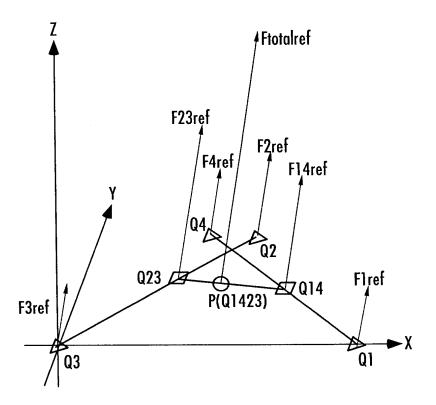
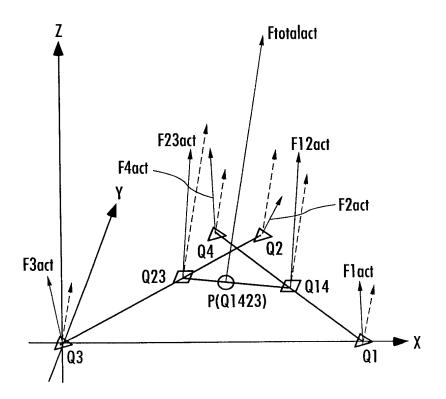
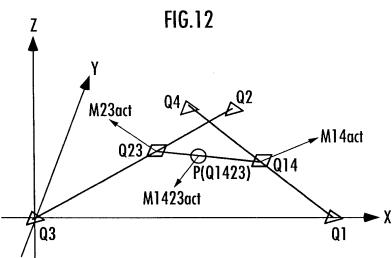


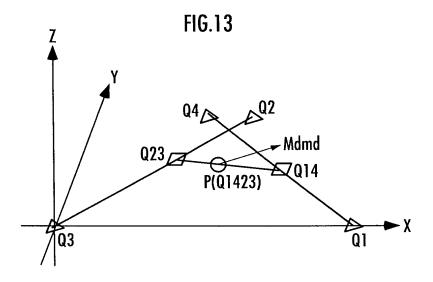
FIG.11

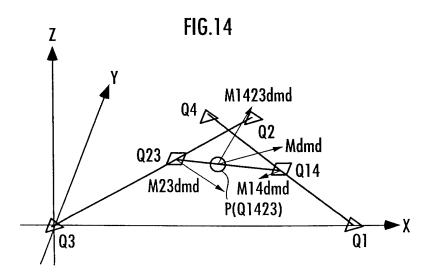


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FIG.15

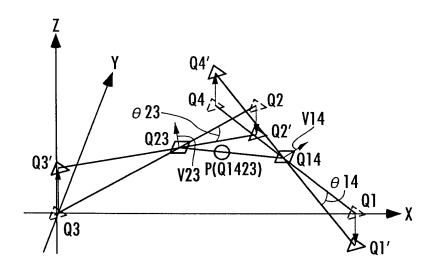
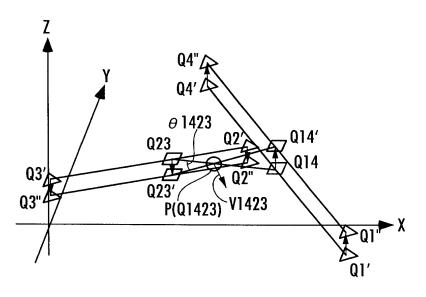


FIG.16



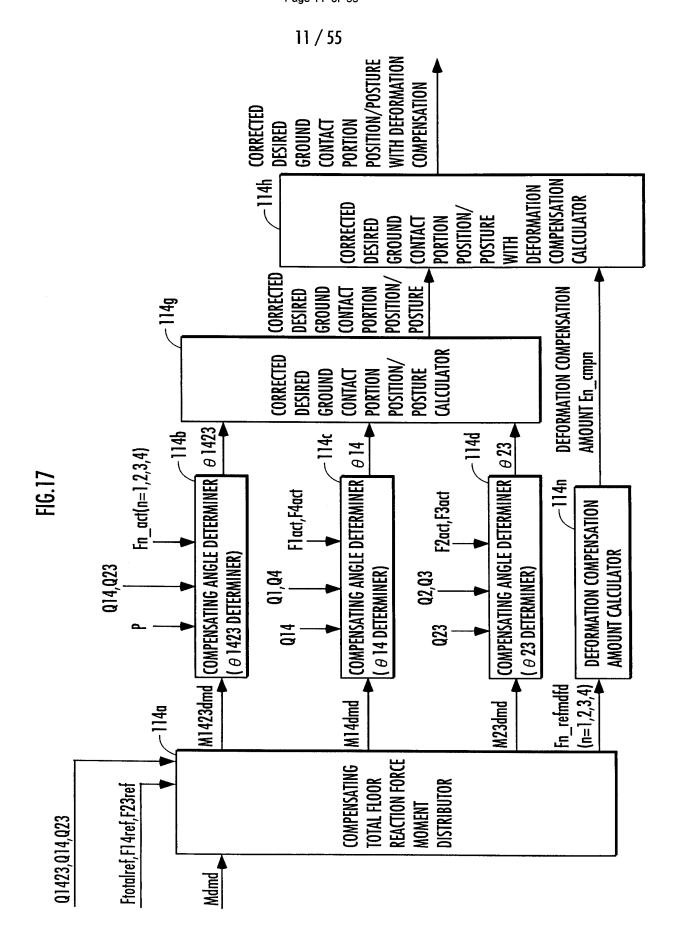
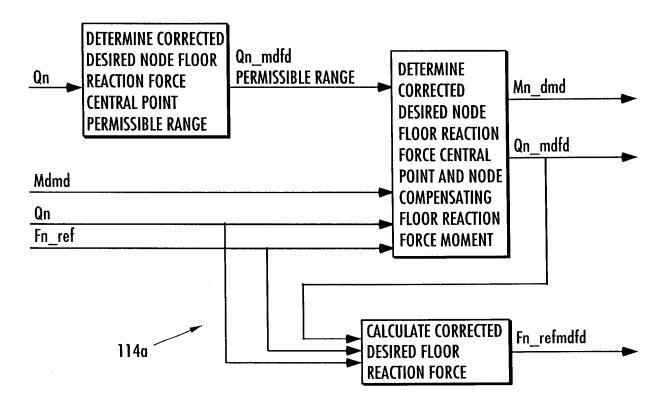
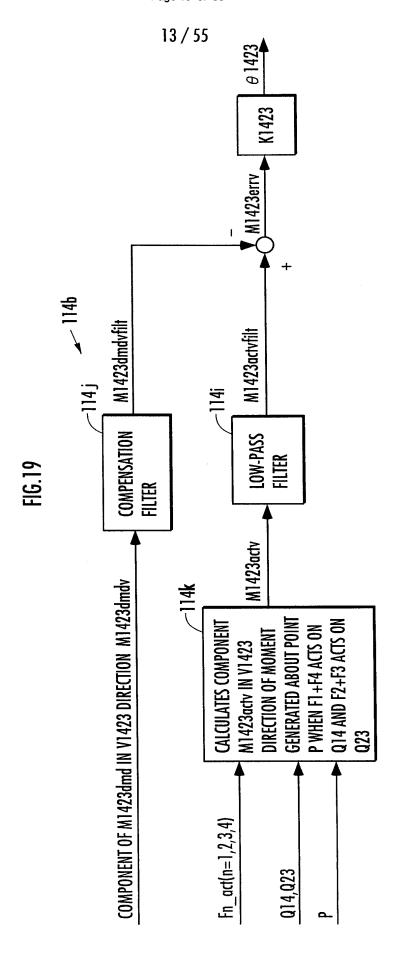
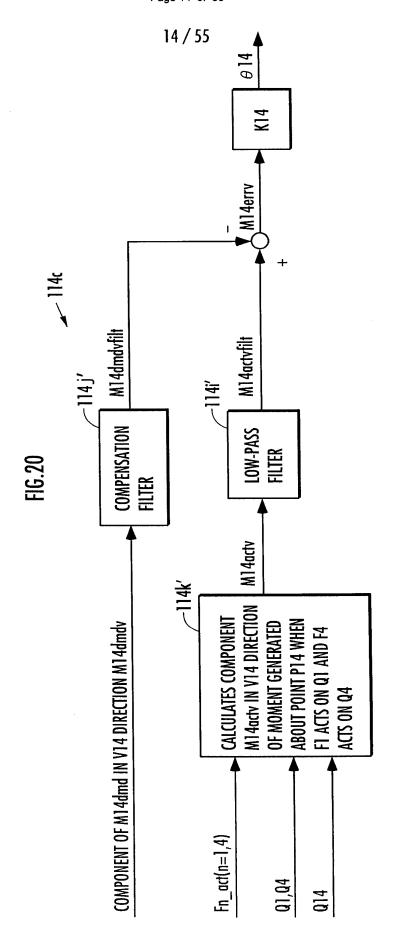


FIG.18

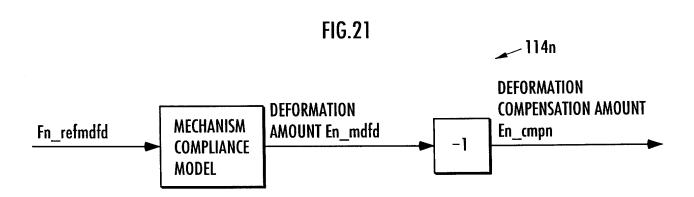




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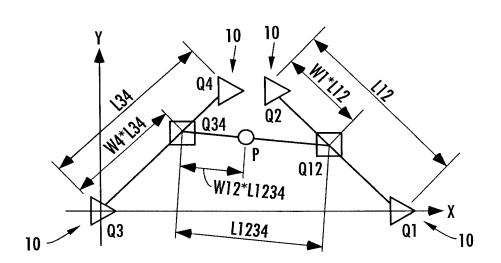
FIG.22

ENTRY \$100 CALCULATE ACTUAL n-TH NODE FLOOR REACTION FORCE Fn_act(n=1,2,3,4,14,23,1423) ON THE BASIS OF ACTUAL FLOOR REACTION FORCE OF EACH GROUND CONTACT PORTION **S102** CALCULATE ACTUAL n-TH NODE FLOOR REACTION FORCE MOMENT Mn_act(n=1,2,3,4,14,23,1423) **S104** DETERMINE n-TH NODE COMPENSATING FLOOR REACTION FORCE MOMENT Mn_dmd(n=14,23,1423) ON THE BASIS OF COMPENSATING TOTAL FLOOR REACTION FORCE MOMENT \$106 DETERMINE VECTORS V1423,V14,V23 AND VECTORS U1423,U14,U23 ORTHOGONAL THERETO, AS DEFINED IN HIERARCHICAL COMPLIANCE OPERATION **S108** EXTRACT COMPONENT IN Vn DIRECTION Mn actv AND COMPONENT IN Un DIRECTION Mn actu OF ACTUAL n-TH NODE FLOOR REACTION FORCE MOMENT (n=14,23,1423) **S110** EXTRACT COMPONENT IN Vn DIRECTION Mn dmdv AND COMPONENT IN Un DIRECTION Mn_dmdu OF n-TH NODE COMPENSATING FLOOR REACTION FORCE MOMENT Mn dmd(n=14,23,1423) **S112** DETERMINE V COMPONENT OF n-TH NODE COMPENSATING ANGLE BY MULTIPLYING DIFFERENCE BETWEEN VALUE OBTAINED BY PASSING Mn acty THROUGH FILTER AND VALUE OBTAINED BY PASSING Mn dmdv THROUGH FILTER BY GAIN Kn **S114** DETERMINE U COMPONENT OF n-TH NODE COMPENSATING ANGLE BY MULTIPLYING DIFFERENCE BETWEEN VALUE OBTAINED BY PASSING Mn_actu THROUGH FILTER AND VALUE OBTAINED BY PASSING Mn_dmdu THROUGH FILTER BY GAIN Kn

RETURN

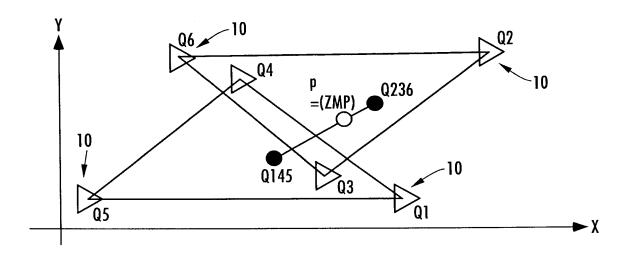
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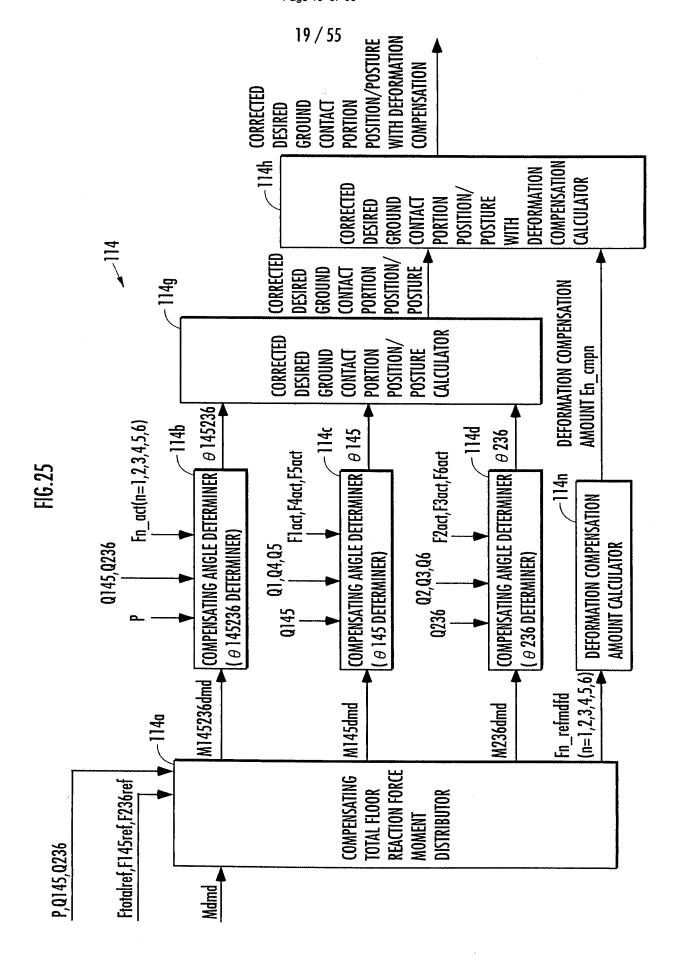
FIG.23



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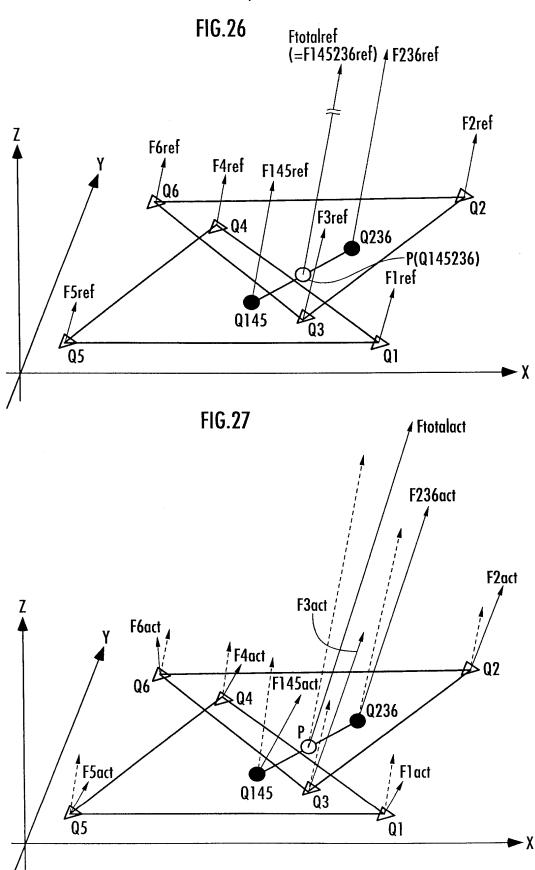
FIG.24





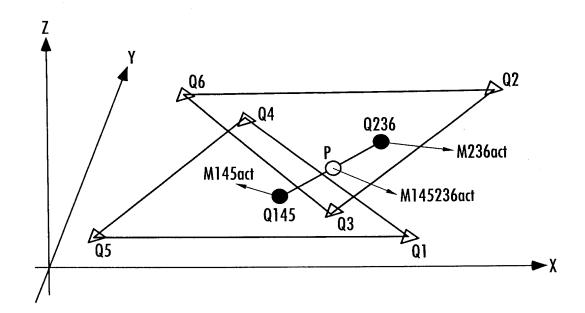
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FIG.28



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FIG.29(a)

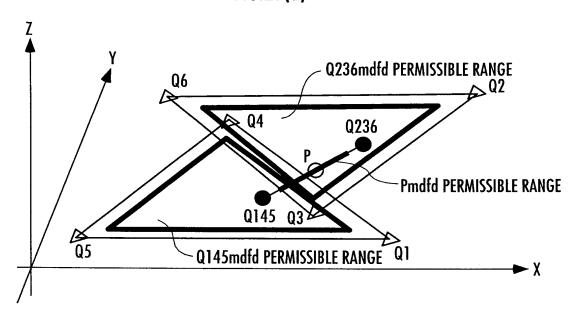
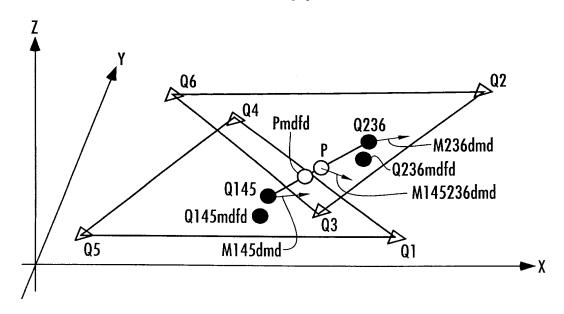


FIG.29(b)



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FIG.30

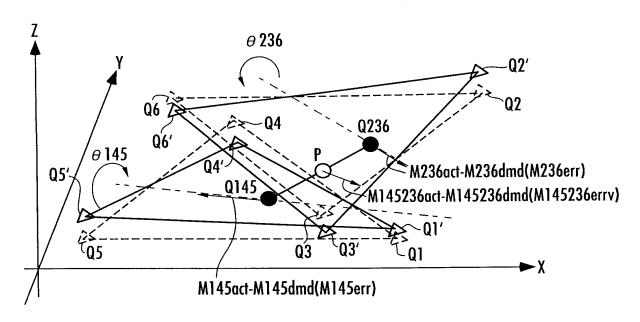
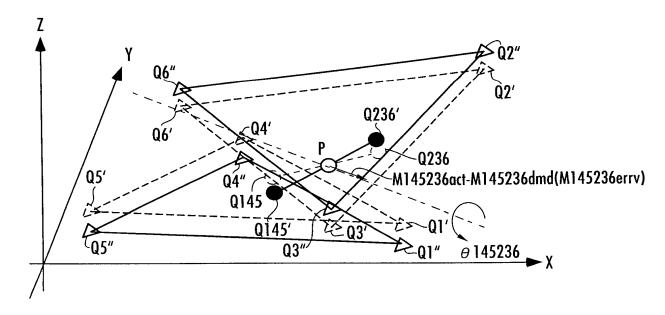
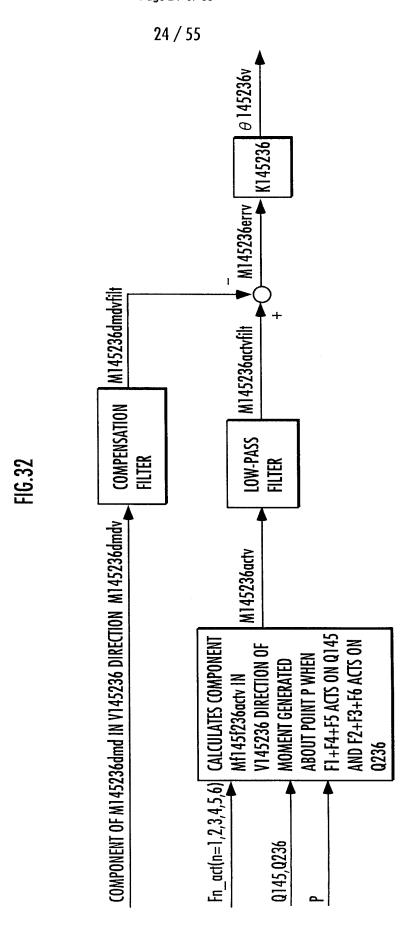
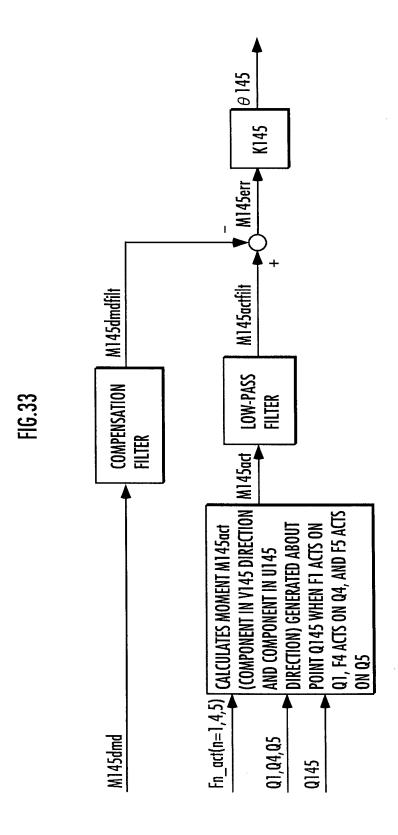


FIG.31



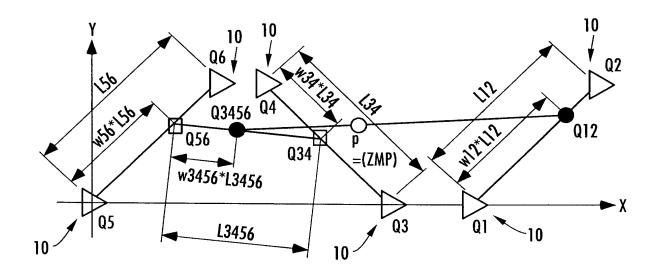


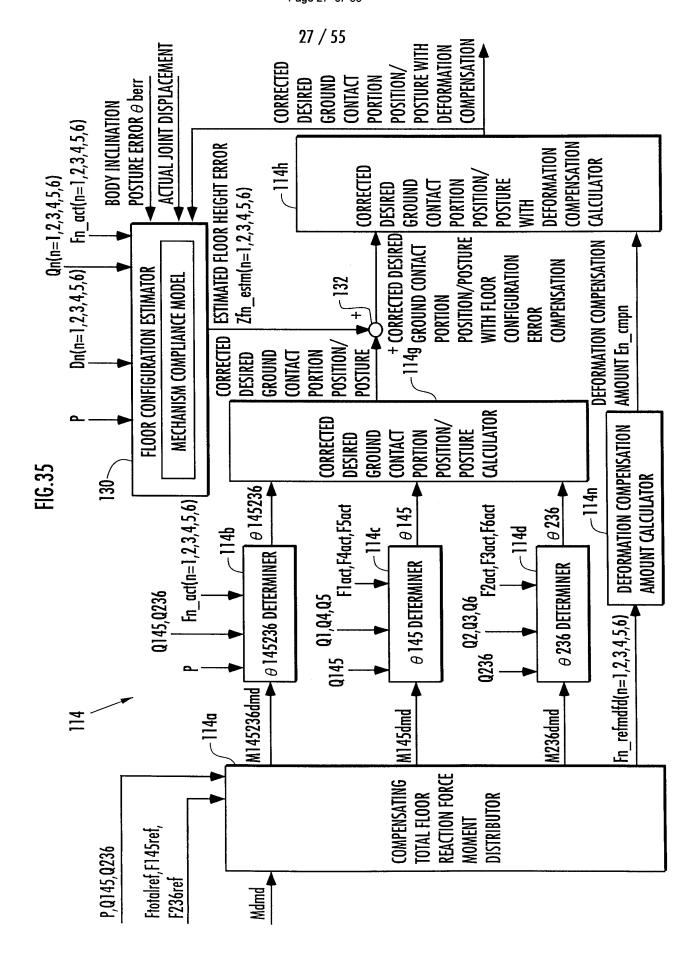
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FIG.34





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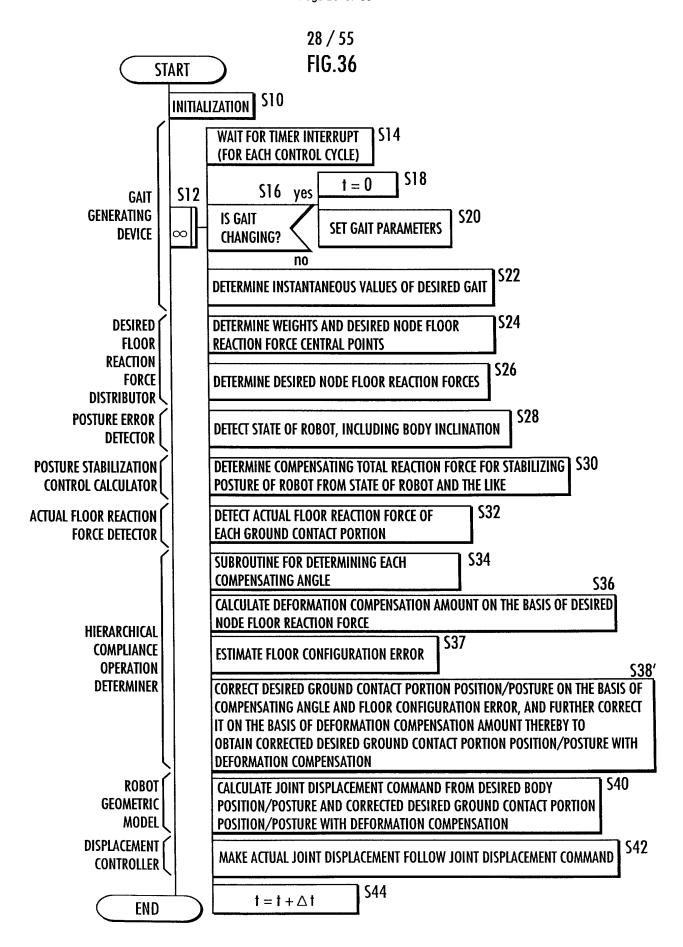


FIG.37

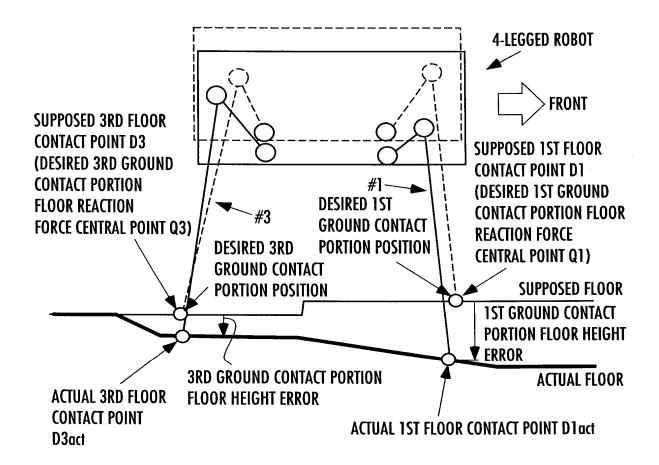
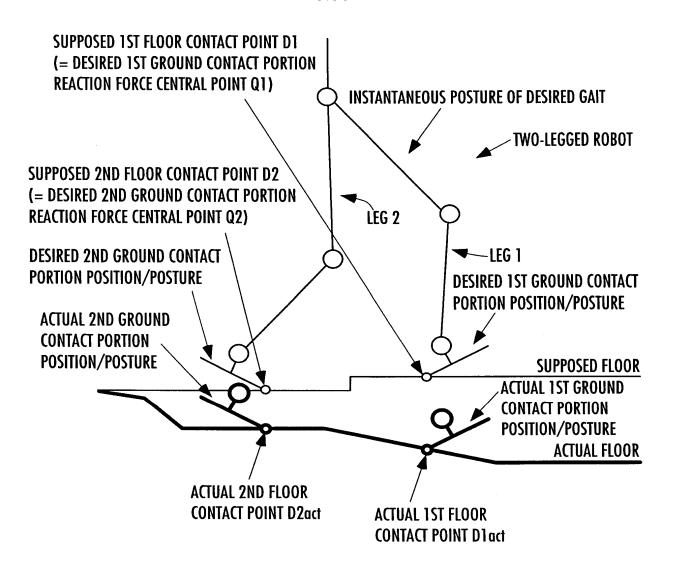


FIG.38



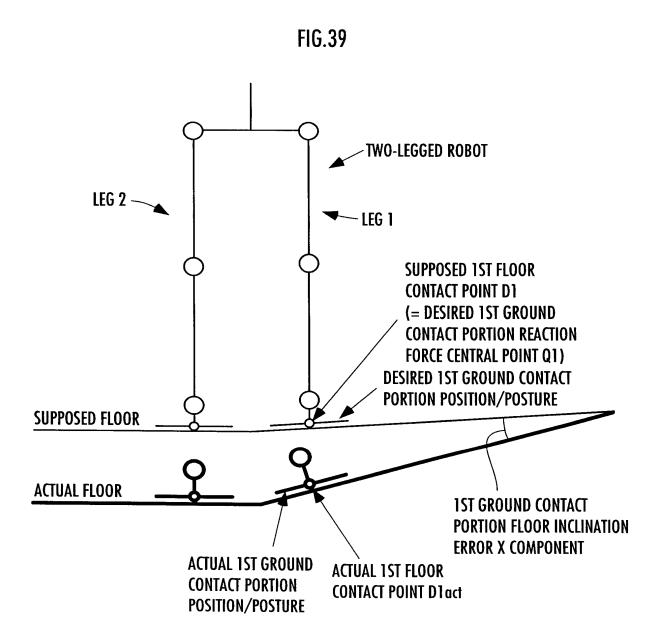


FIG.40

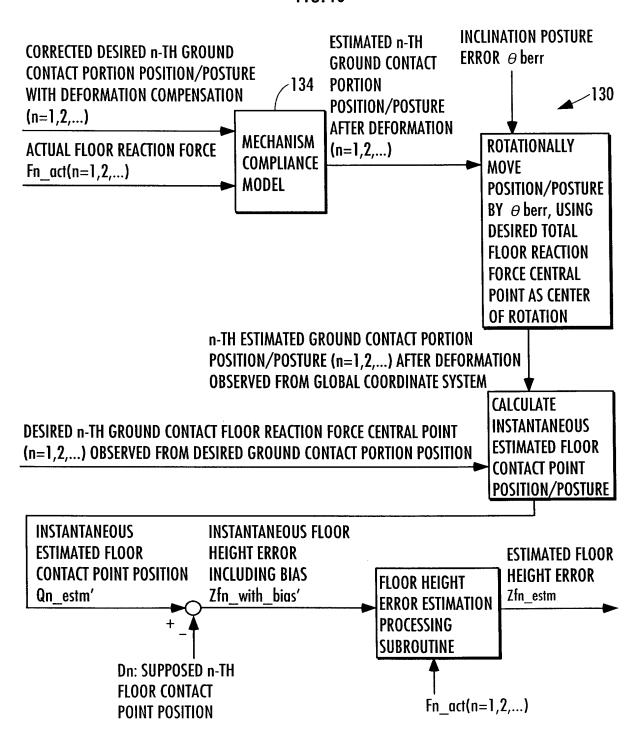


FIG.41

ENTRY

HIERARCHICALLY RELATIVIZE BIAS-INCLUDED INSTANTANEOUS n-TH GROUND CONTACT PORTION FLOOR HEIGHT ERROR Zfn_with_bias' TO DETERMINE INSTANTANEOUS n-TH NODE RELATIVE FLOOR HEIGHT ERROR Zn_rel'

S52

\$50

HIERARCHICALLY RELATIVIZE ESTIMATED n-TH GROUND CONTACT PORTION FLOOR HEIGHT ERROR Zfn_estm_p, WHICH HAS BEEN DETERMINED AT LAST CONTROL CYCLE, BY USING CURRENT WEIGHT TO DETERMINE LAST ESTIMATED n-TH NODE RELATIVE FLOOR HEIGHT ERROR Zn_rel_estm_p

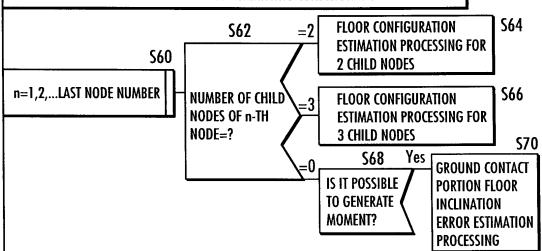
S56

$$Zn_{inc_cand} = (Zn_{rel'} - Zn_{rel_estm_p})$$
* $\triangle T / (Testm + \triangle T)$

DETERMINE NODE REQUEST MODE OF EACH NODE ON THE BASIS OF TIMING OF DESIRED GAIT

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DETERMINE EACH NODE MODE ON THE BASIS OF NODE REQUEST MODE AND RESULT OF DETERMINATION OF WHETHER ESTIMATION PERMITTING CONDITION IS SATISFIED

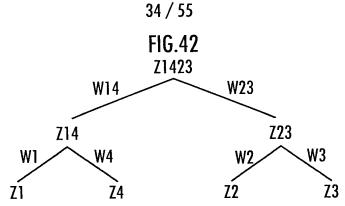


DETERMINE SUM OF ESTIMATED RELATIVE FLOOR HEIGHT ERRORS OF ALL ANCESTOR NODES OF n-TH NODE (n=1,2,...LAST LEAF NODE NUMBER) AND ESTIMATED n-TH NODE RELATIVE FLOOR HEIGHT ERROR, AND DEFINE THE DETERMINED SUM AS ESTIMATED n-TH GROUND CONTACT PORTION FLOOR HEIGHT ERROR Zfn estm

S72

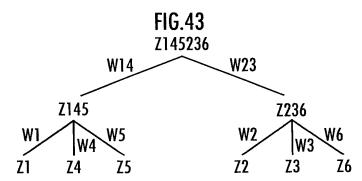
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Z14_with_bias = W1 • Z1_with_bias + W4 • Z4_with_bias
Z23_with_bias = W2 • Z2_with_bias + W3 • Z3_with_bias
Z1423 with_bias = W14 • Z14_with_bias + W23 • Z23_with_bias

Z1_rel = Z1_with_bias - Z14_with_bias
Z4_rel = Z4_with_bias - Z14_with_bias
Z2_rel = Z2_with_bias - Z23_with_bias
Z3_rel = Z3_with_bias - Z23_with_bias
Z14_rel = Z14_with_bias - Z1423_with_bias
Z23_rel = Z23_with_bias - Z1423_with_bias



Z145_with_bias = W1 • Z1_with_bias + W4 • Z4_with_bias + W5 • Z5_with_bias Z236_with_bias = W2 • Z2_with_bias + W3 • Z3_with_bias + W6 • Z6_with_bias Z145236_with_bias = W145 • Z145_with_bias + W236 • Z236_with_bias

Z1_rel = Z1_with_bias - Z145_with_bias
Z4_rel = Z4_with_bias - Z145_with_bias
Z5_rel = Z5_with_bias - Z145_with_bias
Z2_rel = Z2_with_bias - Z236_with_bias
Z3_rel = Z3_with_bias - Z236_with_bias
Z6_rel = Z6_with_bias - Z236_with_bias
Z145_rel = Z145_with_bias - Z145236_with_bias
Z236_rel = Z236_with_bias - Z145236_with_bias

FIG.44

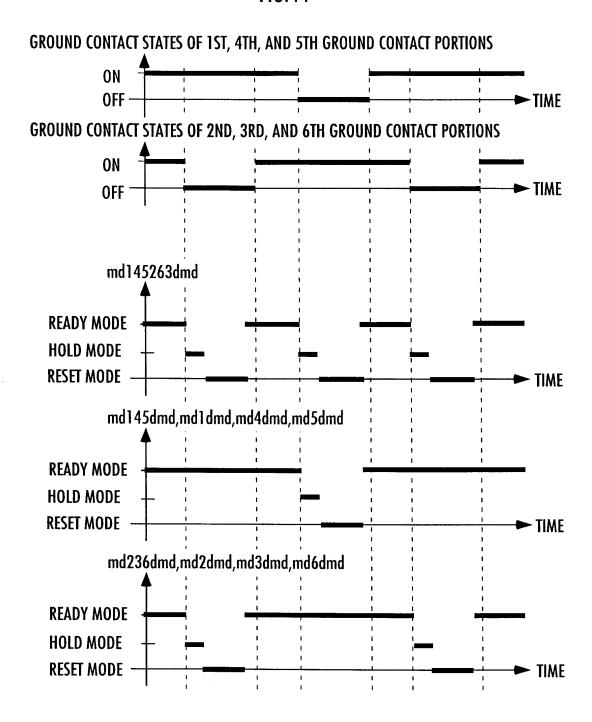
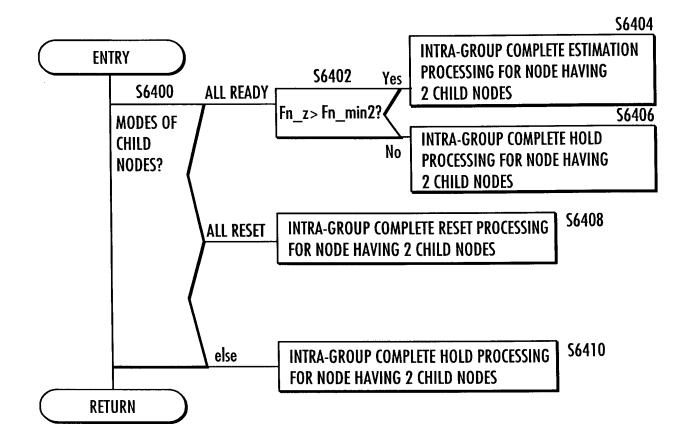
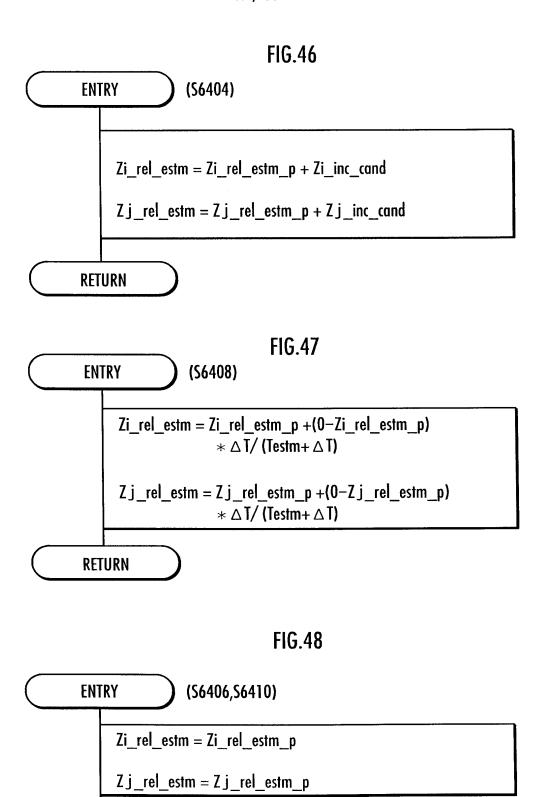


FIG.45

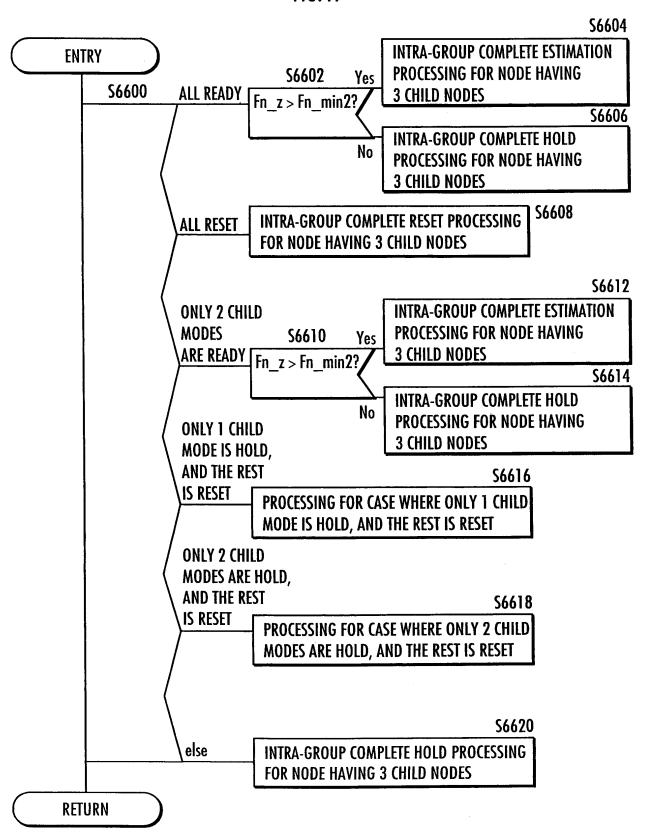




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FIG.49



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FIG.50

Zi_rel_estm = Zi_rel_estm_p + Zi_inc_cand

Z j_rel_estm = Z j_rel_estm_p + Z j_inc_cand

Zk_rel_estm = Zk_rel_estm_p + Zk_inc_cand

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FIG.51

ENTRY

(\$6608)

$$Zi_rel_estm = Zi_rel_estm_p + (0 - Zi_rel_estm_p)$$

 $* \triangle T/(Testm + \triangle T)$

$$Zj_rel_estm = Zj_rel_estm_p + (0 - Zj_rel_estm_p)$$

 $* \Delta T/(Testm + \Delta T)$

$$Zk_rel_estm = Zk_rel_estm_p + (0 - Zk_rel_estm_p)$$

 $* \triangle T/(Testm + \triangle T)$

RETURN

FIG.52

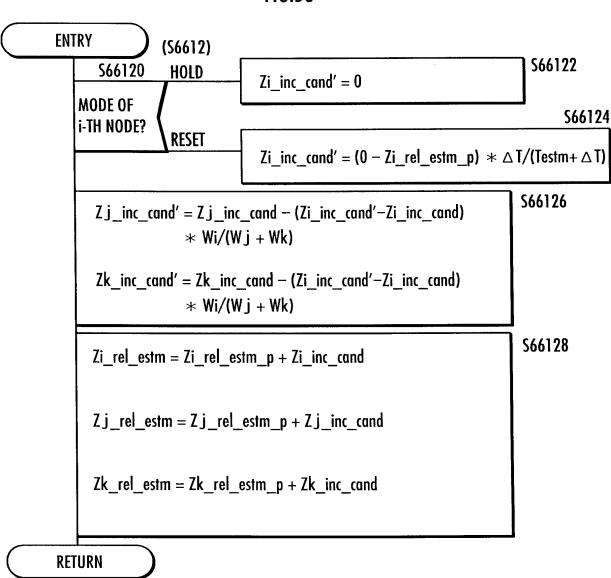
ENTRY

(\$6606,\$6614,\$6620)

$$Zk_rel_estm = Zk_rel_estm_p$$

RETURN

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FIG.54

ENTRY

(\$6616)

$$Zi_rel_estm = 0$$

$$Z_j_rel_estm = Z_j_rel_estm_p + (0 - Z_j_rel_estm_p)$$

 $* \Delta T/(Testm + \Delta T)$

$$\begin{split} Zk_rel_estm &= Zk_rel_estm_p + (0 - Zk_rel_estm_p) \\ &\quad * \triangle T/(+ \triangle T) \end{split}$$

RETURN

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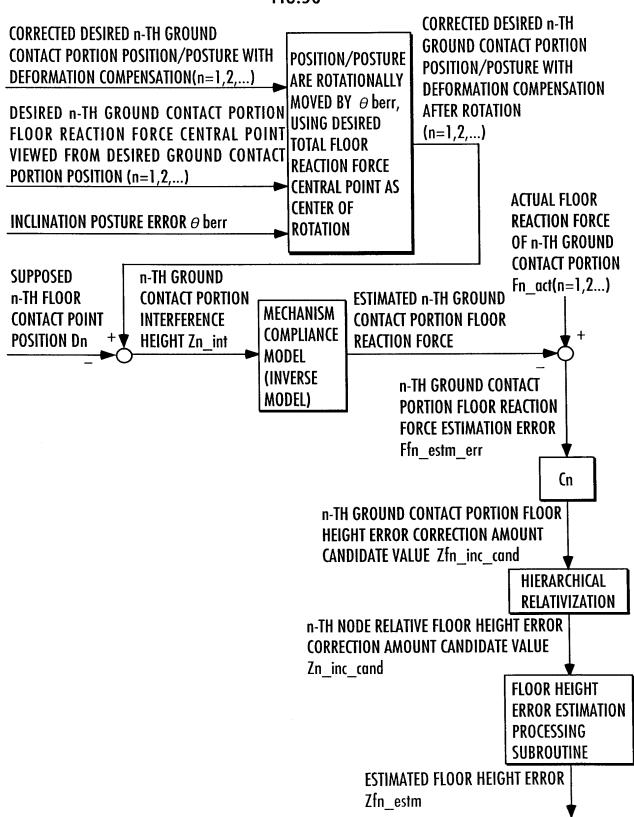
FIG.55

| Zi_rel_estm = Zi_rel_estm_p
| Zj_rel_estm = Zj_rel_estm_p
| Zk_rel_estm = Zk_rel_estm_p + (0 - Zk_rel_estm_p)
| * ΔT/(Testm+ΔT)

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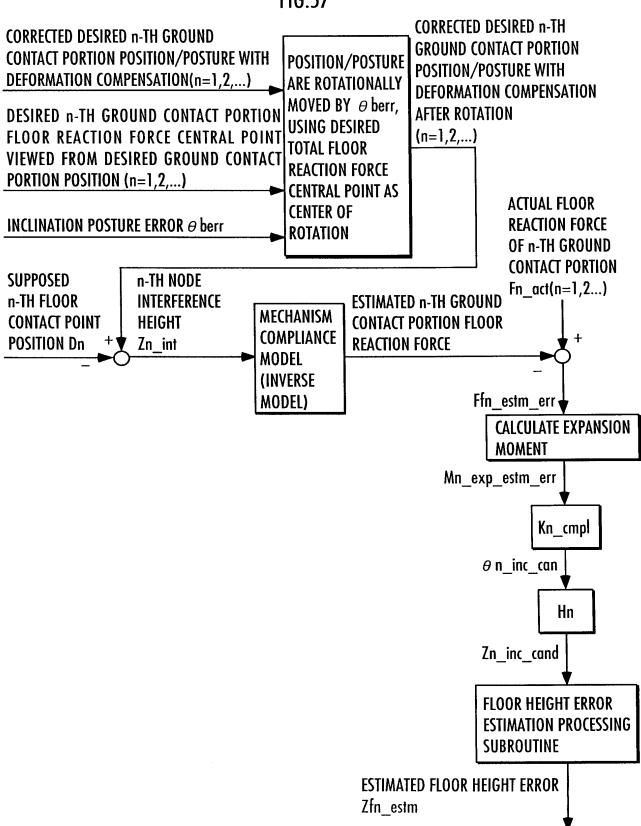
FIG.56

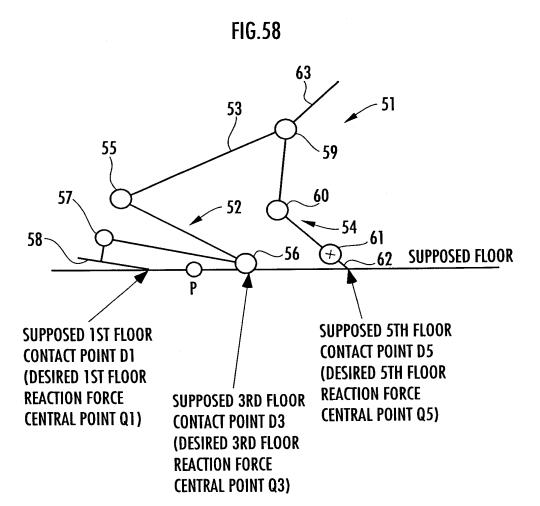


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FIG.57

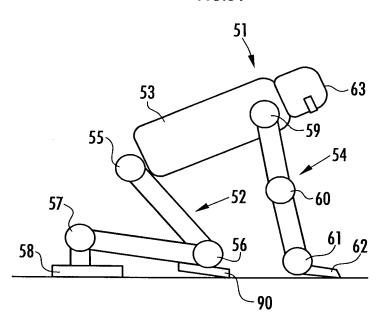




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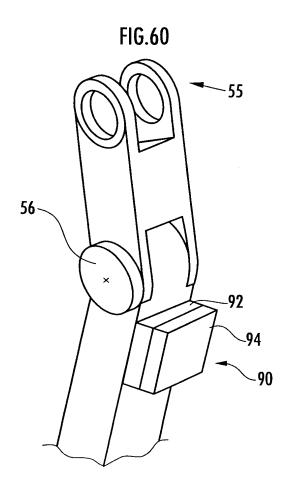
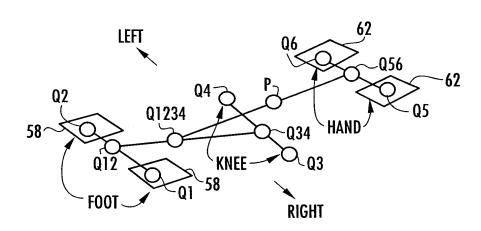
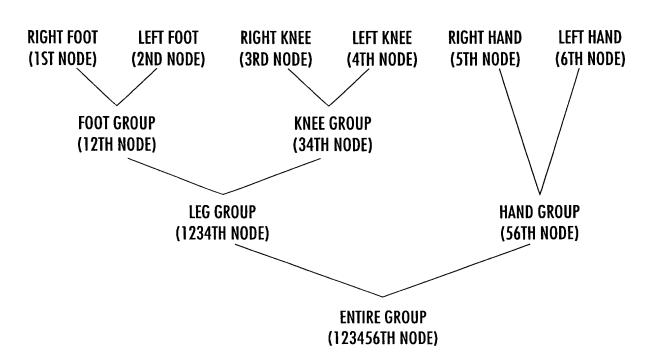
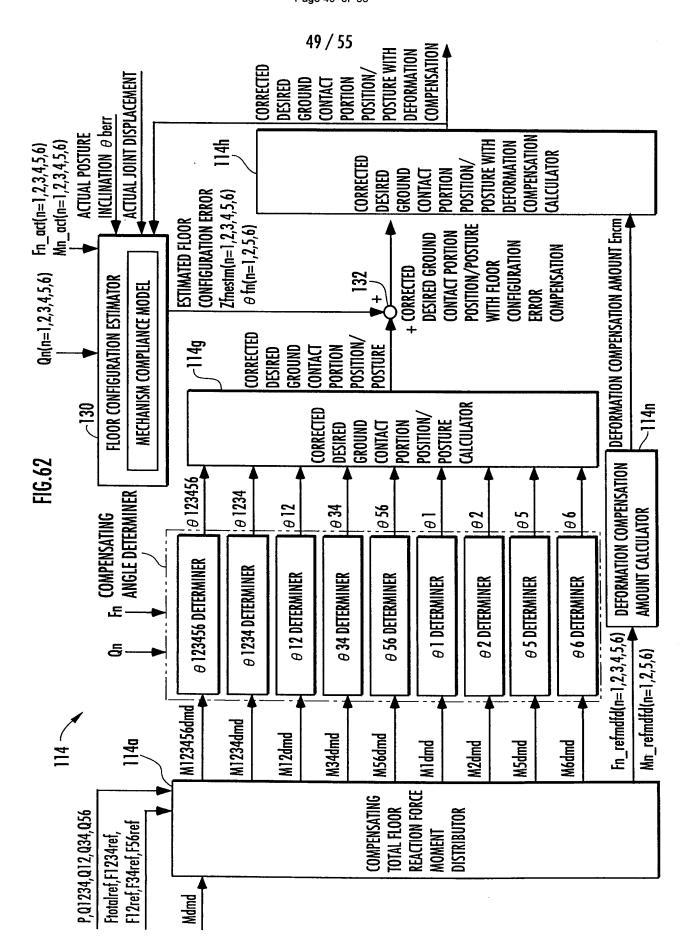


FIG.61







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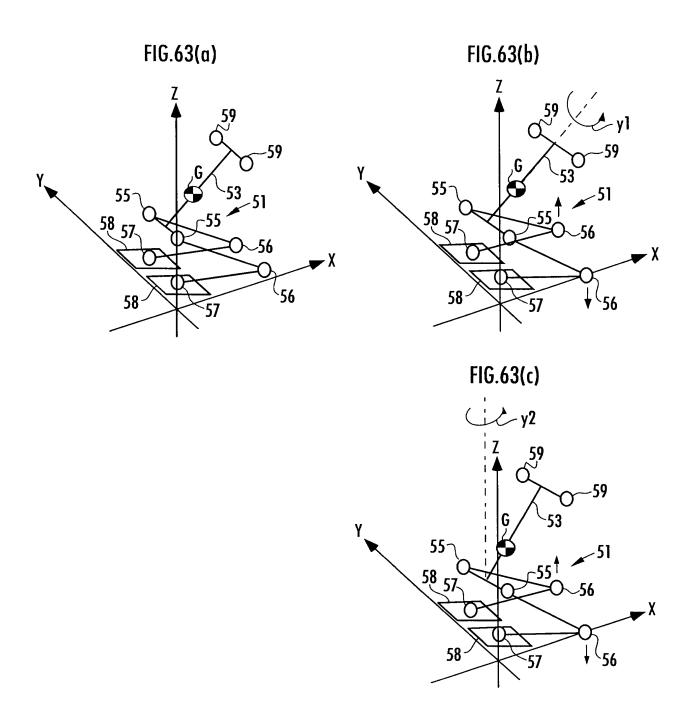
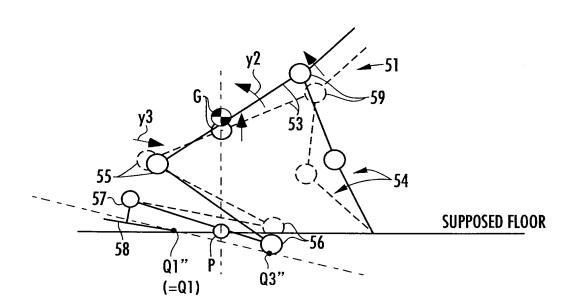
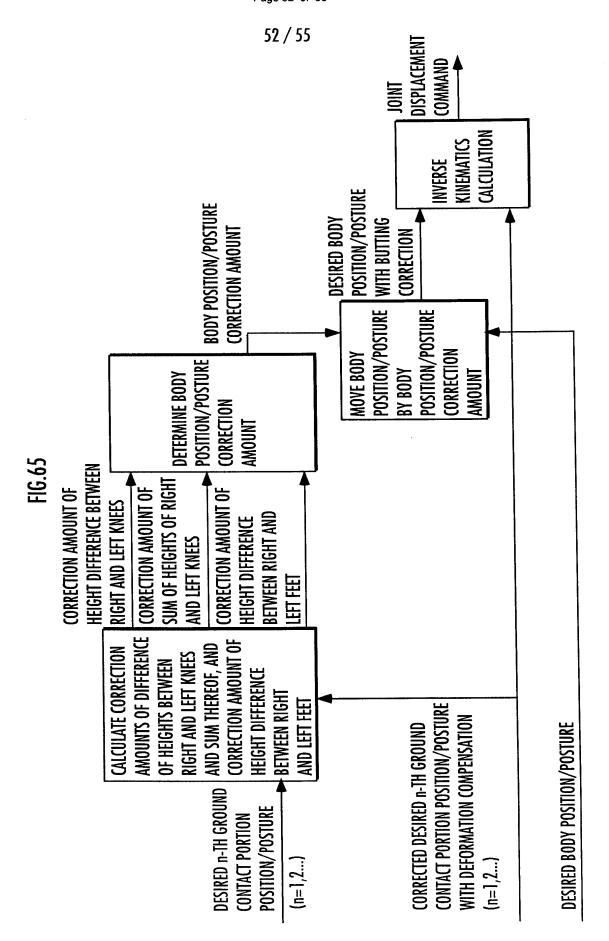


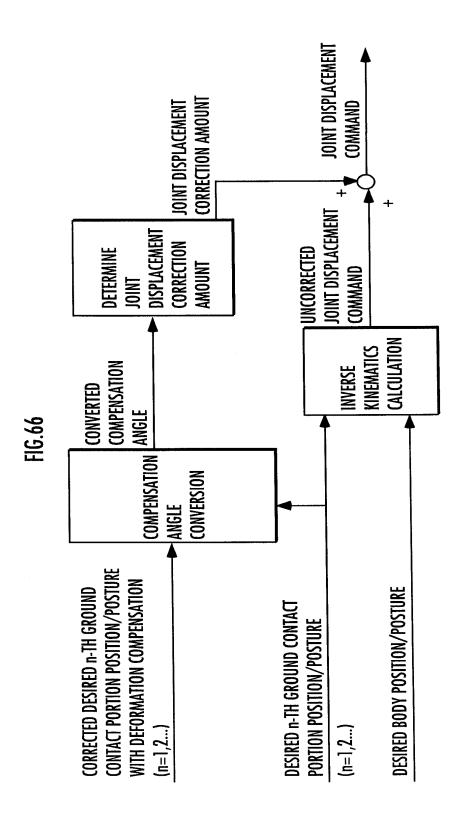
FIG.64



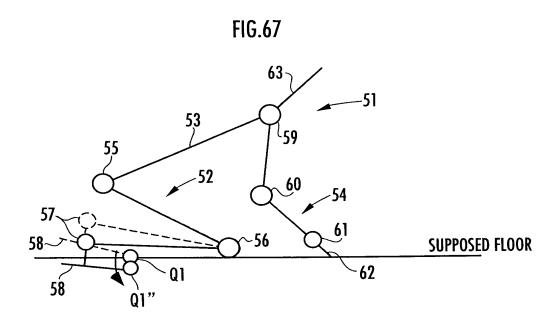
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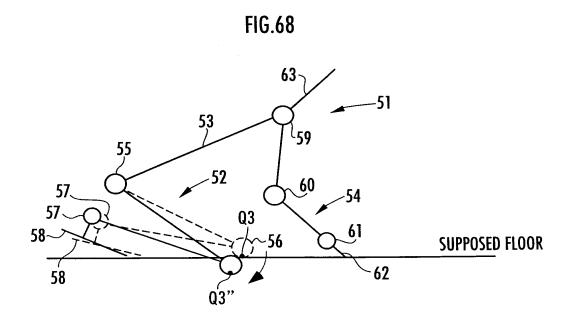


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